

# Introduction

ThermaFoam R-Control Geofoam is used in a wide range of structural and civil engineering applications. The selection of the appropriate grade of ThermaFoam R-Control Geofoam for a specific application is a critical decision to ensure suitable long term performance.

ThermaFoam R-Control Geofoam is a structural material produced in compliance with ASTM D6817, "Standard Specification for Rigid Cellular Geofoam". ThermaFoam R-Control Geofoam is available in 7 standard grades with compressive resistance @1 % strain ranging from 320 to 2,680 psf where the compressive resistance at 1% is the industry accepted allowable stress for the combination of dead and live loads for geofoam.

# Disclaimer

This geofoam selection example is being provided to illustrate a simplified method for the calculation of vertical stress on geofoam in a hypothetical example. This simplified method is being provided only as an example and should not be relied upon for the selection of ThermaFoam R-Control Geofoam for a particular project. In applications where a concrete load distribution slab is used above the geofoam, more advanced load distribution analysis methods such as finite element modeling are recommended.

The selection and/or specification of a ThermaFoam R-Control Geofoam grade for a specific application should be determined by a qualified civil engineer who is acquainted with all possible aspects of a particular project.

# Example

A project is proposed to be built using geofoam with a cross section and loads as shown in Figure 1. ThermaFoam R-Control Geofoam EPS 22 Geofoam is proposed to be used. Vertical loads must be calculated to ensure ThermaFoam R-Control Geofoam EPS 22 Geofoam is appropriate.

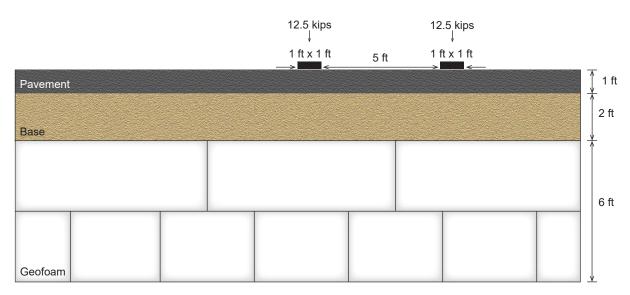


Figure 1. Project Section





# **Analysis Method**

A simplified vertical stress distribution model is shown in Figure 2 and Figure 3 based on NCHRP published literature<sup>1</sup>.

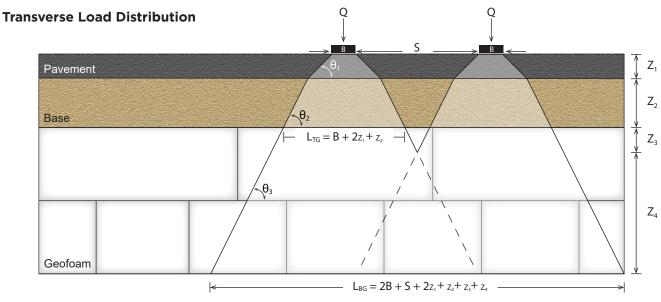
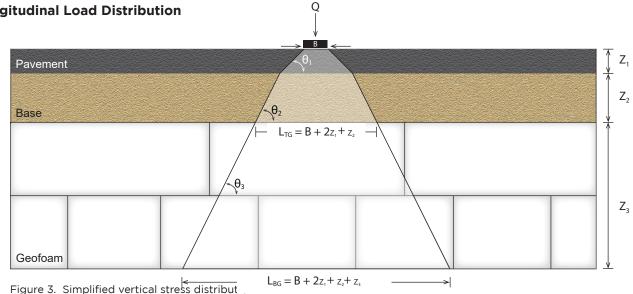


Figure 2. Simplified vertical stress distribution



- Q = loading
- B = equivalent width of loading in the transverse or longitudinal direction
- S = spacing between inside edge of equivalent width of loading
- $\theta_1 = 1H:1V$  slope
- $\theta_2 = 1H:2V$  slope
- $\theta_3 = 1H:2V$  slope
- $z_1$  = thickness of pavement
- $z_2$  = thickness of road base
- $z_3$  = depth within geofoam
- $z_4$  = depth within geofoam

Reference

<sup>1</sup>NCHRP Web Document 65 (Project 24-11) Geofoam Applications in Design and Construction of Highway Embankments, National Cooperative Highway Research Program, July 2004

# **Longitudinal Load Distribution**

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#### **Calculation - Dead Loads**

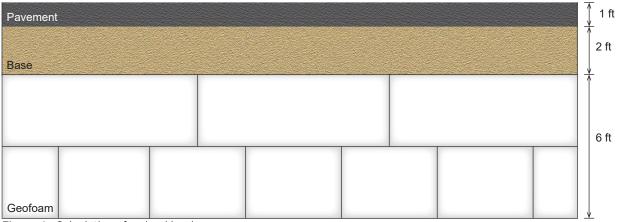


Figure 4. Calculations for dead loads

Dead load at top of geofoam:

 $\sigma_{\text{DL TG}}$  =  $z_1 * \gamma_{\text{Pavement}} + z_2 * \gamma_{\text{Base}}$ 

where  $\gamma_{\text{Pavement}}$  and  $\gamma_{\text{Base}}$  = unit weight of pavement and base, respectively

$$\begin{split} \sigma_{\text{\tiny DL\,TG}} = 1\,\text{ft} * 145\,\text{lbs/ft}^3 + 2\,\text{ft} * 140\,\text{lbs/ft}^3 = 425\,\text{lbs/ft}^2 \\ \sigma_{\text{\tiny DL\,TG}} = (425\,\text{lbs/ft}^3)\,/\,(144\,\text{in}^2/\text{ft}^2) = 2.95\,\text{psi} \end{split}$$

Dead load at beginning of overlap depth of geofoam: (see Figure 5)

 $\sigma_{\text{DL BG}} = z_1 * \gamma_{\text{Pavement}} + z_2 * \gamma_{\text{Base}} + z_{\text{GEOFOAM}} * \gamma_{\text{GEOFOAM}}$ 

where  $\gamma_{Pavement}$  and  $\gamma_{Base}$  and  $\gamma_{GEOFOAM}$  = unit weight of pavement, base, and geofoam, respectively

$$\begin{split} &\sigma_{\rm DL\,BG} = 1~{\rm ft}~{}^*~145~{\rm lbs/ft}^3 + 2~{\rm ft}~{}^*~140~{\rm lbs/ft}^3 + 1~{\rm ft}~{}^*~1.35~{\rm lbs/ft}^3 = 426~{\rm lbs/ft}^2 \\ &\sigma_{\rm DL\,BG} = (426~{\rm lbs/ft}^2)~/~(144~{\rm in}^2/{\rm ft}^2) = 2.96~{\rm psi} \end{split}$$

Dead load at bottom of geofoam:

 $\sigma_{\text{dl BG}} = z_1 * \gamma_{\text{Pavement}} + z_2 * \gamma_{\text{Base}} + z_{\text{GEOFOAM}} * \gamma_{\text{GEOFOAM}}$ 

where  $\gamma_{Pavement}$  and  $\gamma_{Base}$  and  $\gamma_{GEOFOAM}$  = unit weight of pavement, base, and geofoam, respectively

$$\begin{split} &\sigma_{\rm DL\,BG} = 1~{\rm ft}~{*}~145~{\rm lbs/ft^3} + 2~{\rm ft}~{*}~140~{\rm lbs/ft^3} + 6~{\rm ft}~{*}~1.35~{\rm lbs/ft^3} = 433~{\rm lbs/ft^2} \\ &\sigma_{\rm DL\,BG} = (433~{\rm lbs/ft^2})~/~(144~{\rm in^2/ft^2}) = 3.01~{\rm psi} \end{split}$$



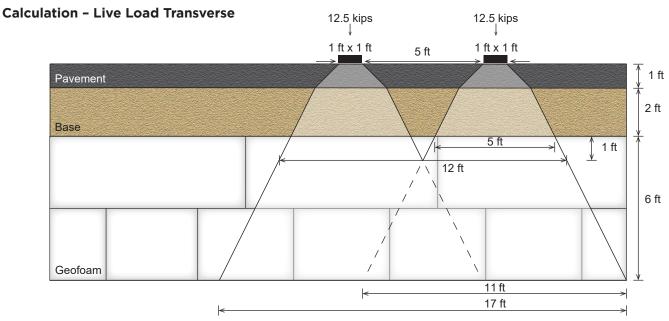


Figure 5. Calculations for live loads

Live load width at top of geofoam:

 $L_{TG} = B + 2z_1 + z_2$  $L_{TG} = 1 \text{ ft} + 2 * 1 \text{ ft} + 2 \text{ ft} = 5 \text{ ft}$ 

Live load width at beginning of overlap depth of vertical stress distributions from 2 transverse surface loads

 $L_{\text{OD}} = 2B + S + 2z_1 + z_2 + z_3$  $L_{\text{OD}} = 2 * 1 \text{ ft} + 5 \text{ ft} + 2 * 1 \text{ ft} + 2 \text{ ft} + 1 \text{ ft} = 12 \text{ ft}$ 

Live load width at bottom of geofoam:

$$L_{BG} = 2B + S + 2z_1 + z_2 + z_3 + z_4$$
  
$$L_{BG} = 2 * 1 \text{ ft} + 5 \text{ ft} + 2 * 1 \text{ ft} + 2 \text{ ft} + 1 \text{ ft} + 5 \text{ ft} = 17 \text{ ft}$$

Note: Loads are shown calculated at top, beginning of overlap, and bottom of geofoam only here for simplicity, but the load at any depth in geofoam can be calculated following a similar method.

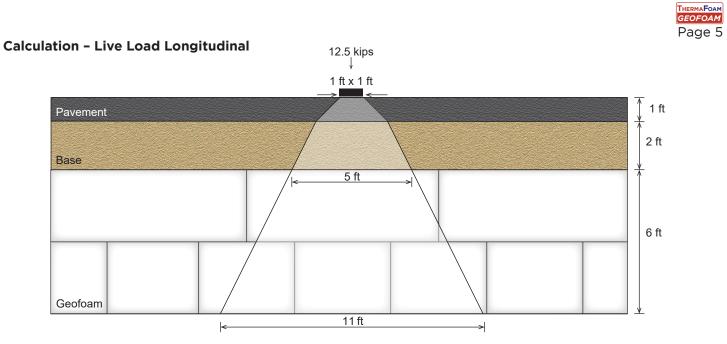


Figure 6. Calculations for live loads

Live load width at top of geofoam:

 $L_{TG} = B + 2z_1 + z_2$  $L_{TG} = 1 \text{ ft} + 2 * 1 \text{ ft} + 2 \text{ ft} = 5 \text{ ft}$ 

Live load width at bottom of geofoam:

$$L_{BG} = B + 2_{Z_1} + _{Z_2} + _{Z_3}$$
$$L_{BG} = 1 \text{ ft} + 2 \text{ * 1 ft} + 2 \text{ ft} + 6 \text{ ft} = 11 \text{ ft}$$

Note: Loads are shown calculated at top and bottom of geofoam only here for simplicity, but the load at any depth in geofoam can be calculated following a similar method.



# **Calculation - Live Loads**

Live load at top of geofoam:

No load interaction so load = Q

$$\begin{split} &\sigma_{\rm LL\,TG} = Q \ / \ (L_{\rm TG\,TR} \ ^* \ L_{\rm TG\,LO}) \\ &\sigma_{\rm LL\,TG} = 12500 \ lb \ / \ (5 \ ft \ ^* \ 5 \ ft) = 500 \ lb \ / \ ft^2 \\ &\sigma_{\rm LL\,TG} = (500 \ lb \ / \ ft^2) \ / \ (144 \ in^2 \ / \ ft^2) = 3.47 \ psi \end{split}$$

Live load at beginning of stress overlap depth of geofoam:

Two loads interact so load = 2Q

$$\begin{split} &\sigma_{\rm LL\,BG} = 2Q \ / \ (L_{\rm OD\,TR} \ ^* \ L_{\rm OD\,LO}) \\ &\sigma_{\rm LL\,BG} = 2 \ ^* \ 12500 \ lb \ / \ (12 \ ft \ ^* \ 6 \ ft) \ / \ = \ 347 \ lb \ / \ ft^2 \\ &\sigma_{\rm LL\,BG} = (347 \ lb \ / \ ft^2) \ / \ (144 \ in^2 \ / \ ft^2) = \ 2.41 \ psi \end{split}$$

Live load at bottom of geofoam:

$$\begin{split} &\sigma_{\text{LL BG}} = 2\text{Q} / (\text{L}_{\text{BG TR}} * \text{L}_{\text{BG LO}}) \\ &\sigma_{\text{LL BG}} = 2 * 12500 \text{ lb} / (17 \text{ ft} * 11 \text{ ft}) / = 134 \text{ lb}/\text{ft}^2 \\ &\sigma_{\text{LL BG}} = (134 \text{ lb}/\text{ft}^2) / (144 \text{ in}^2/\text{ft}^2) = 0.93 \text{ psi} \end{split}$$

Maximum stress on Geofoam is 6.42 psi EPS 22 with a compressive resistance at 1% strain of 7.3 psi is suitable.

# **Calculation – Total Dead Loads and Live Loads**

Total load at top of geofoam:

 $\sigma_{_{TL TG}} = \sigma_{_{DL TG}} + \sigma_{_{LL TG}}$  $\sigma_{_{TL TG}} = 425 \text{ lb/ft}^2 + 500 \text{ lb/ft}^2 = 925 \text{ lb/ft}^2$  $\sigma_{_{TL TG}} = 2.95 \text{ psi} + 3.47 \text{ psi} = 6.42 \text{ psi}$ 

Total load at beginning of stress overlap depth of geofoam:

$$\begin{split} &\sigma_{\text{TL ID}} = \sigma_{\text{DL ID}} + \sigma_{\text{LL ID}} \\ &\sigma_{\text{TL ID}} = 426 \text{ lb/ft}^2 + 347 \text{ lb/ft}^2 = 773 \text{ lb/ft}^2 \\ &\sigma_{\text{TL ID}} = 2.96 \text{ psi} + 2.41 \text{ psi} = 5.37 \text{ psi} \end{split}$$

Total load at bottom of geofoam:

 $\sigma_{TL BG} = \sigma_{DL BG} + \sigma_{LL BG}$  $\sigma_{TL BG} = 433 \text{ lb/ft}^2 + 134 \text{ lb/ft}^2 = 567 \text{ lb/ft}^2$  $\sigma_{TL BG} = 3.01 \text{ psi} + 0.93 \text{ psi} = 3.94 \text{ psi}$ 



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